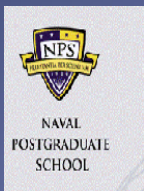


Coordinated Path Following of Multiple UAVs for Time-Critical Missions in the Presence of Time-Varying Communication Topologies



NPS: I. Kaminer, V. Dobrokhodov

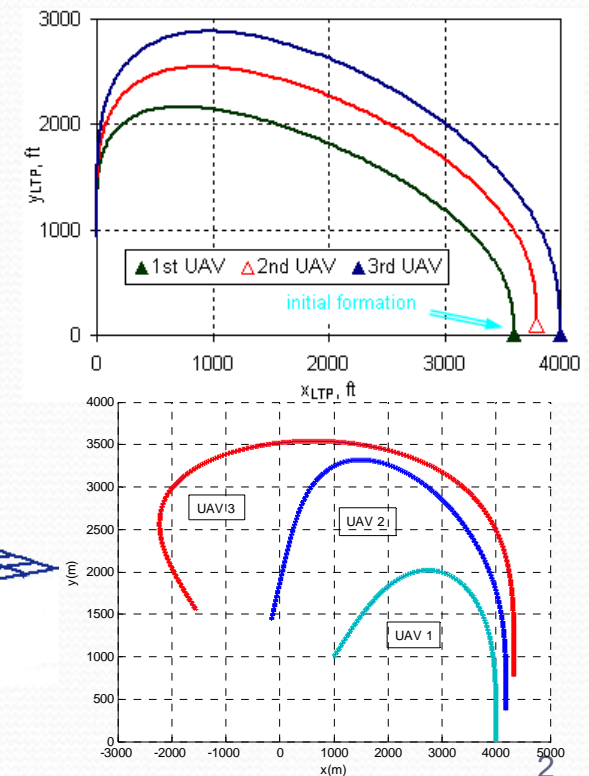
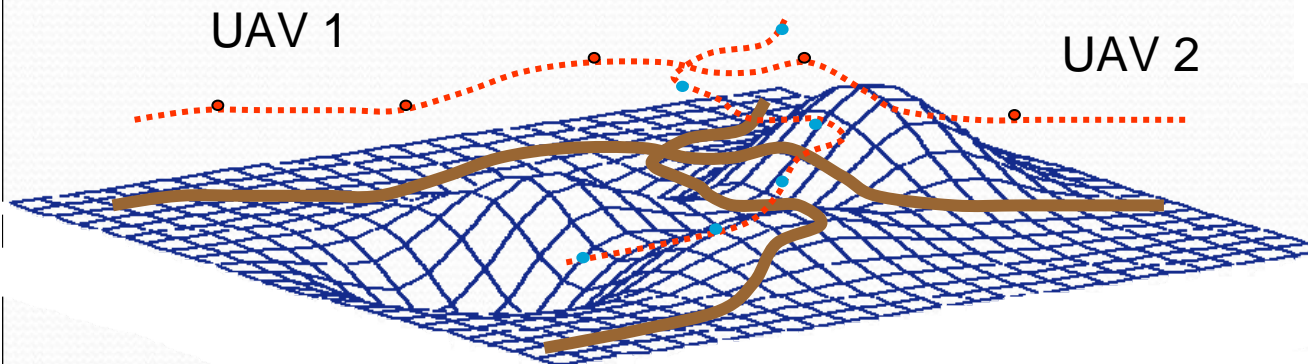
IST: A. Pascoal, A. Aguiar, R. Ghabcheloo

VPI: N. Hovakimyan, E. Xargay, C. Cao



The 17th IFAC World Congress
July 6-11, 2008, Seoul, Korea

- Time Critical Applications for Multiple UAVs with spatial constraints
 - Sequential Autoland
 - Coordinated Reconnaissance – synchronized high resolution pictures
 - Coordinated Road Search
- Coordinate on the arrival of the leader subject to deconfliction, network and spatial constraints





- An integrated solution to **time-critical coordination** problems that includes

- **real-time (RT) path generation** accounting for

- vehicle dynamics plus spatial and temporal coordination constraints

- **nonlinear path following** that relies on UAV attitude to follow the given path – leaving speed along the path as a degree of freedom

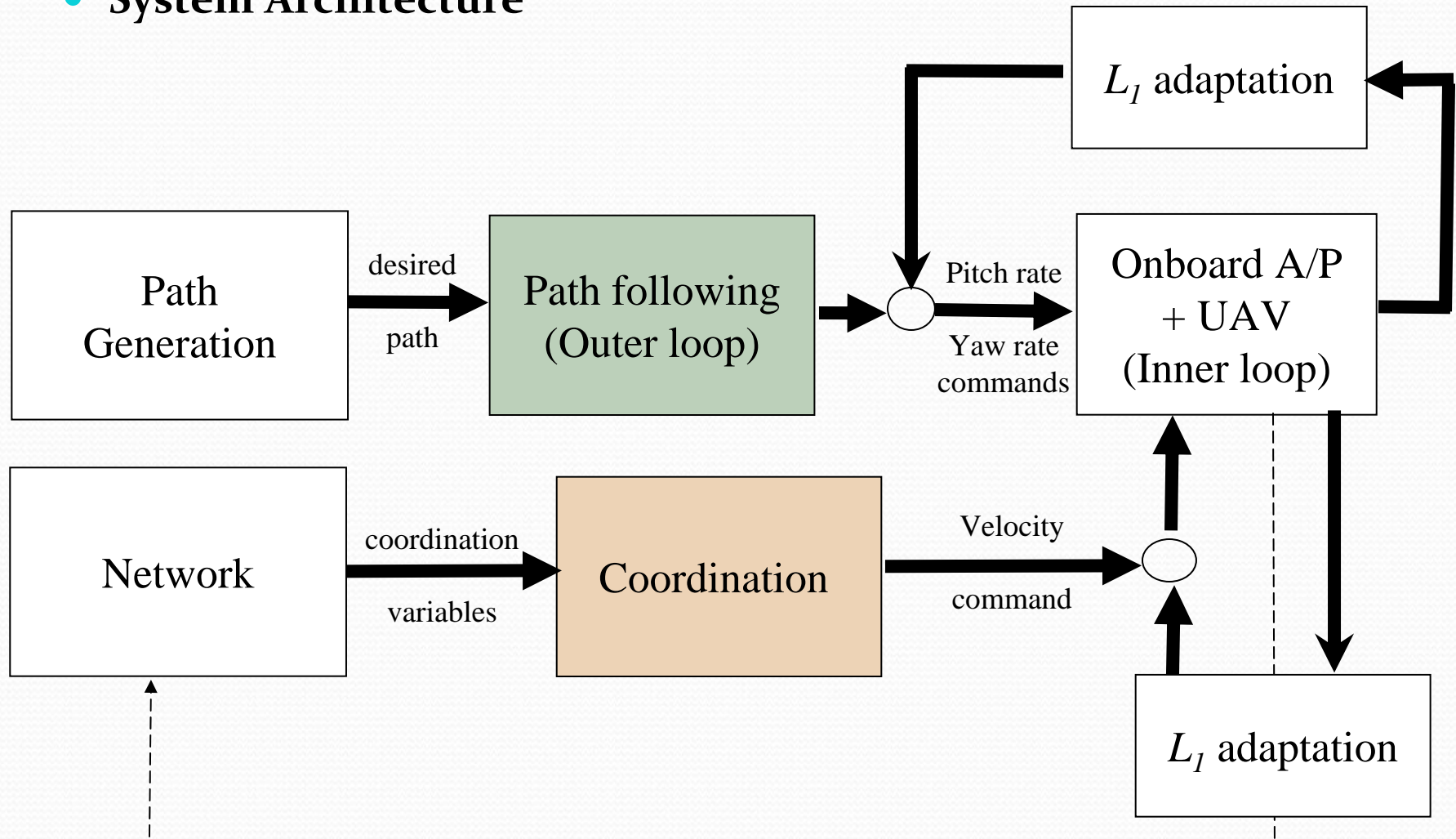


- **L_1 adaptation** to augment off-the-shelf autopilot to enable it to follow the paths it was not designed to follow

(a RT generated path is significantly more “aggressive” than a typical waypoint path these autopilots are designed to follow)

- **Time-critical coordination** controlling the speed of each vehicle over time varying faulty networks to provide robustness – account for the uncertainties that cannot be addressed in the path generation step

- System Architecture



Time Critical Coordination: RT Path Planning

- Assume polynomial paths
- *Decouple space and time in problem formulation* – drastic reduction in the number of optimization parameters (suitable for RT implementation), i.e let

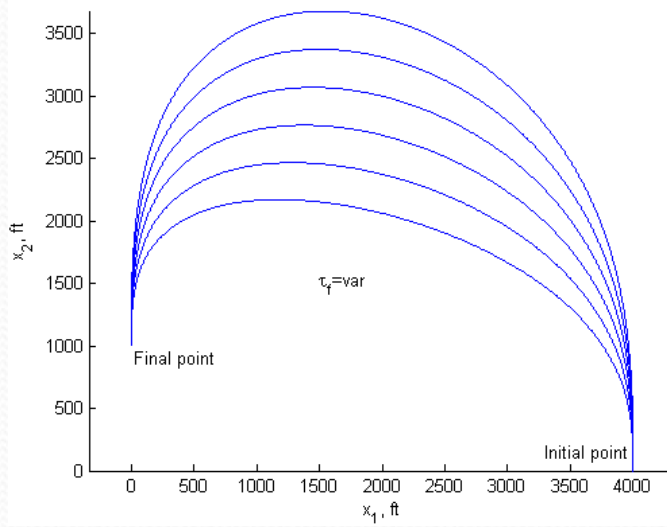
$p_c(\tau) := [x_1(\tau), x_2(\tau), x_3(\tau)]^T$ where $\tau \in [0; \tau_f]$ is e.g. virtual arc length

- $$x_i(\tau) = \sum_{k=0}^N a_{ik} \tau^k$$

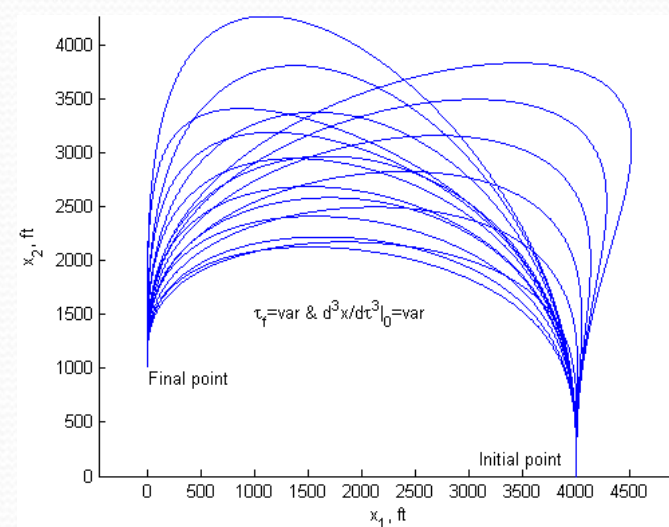
Impact Critical Coordination: RT Path Planning

Table 1. Examples of computation of the coefficients of polynomial trajectories

Boundary conditions	$x_{i0}, x'_{i0}, x''_{i0}, x_{if}, x'_{if}, x''_{if}$					
d_0/d_f	2/2			3 (adding fictitious jerk x''_{i0})/2		
N^*/N	5/5			5/6		
Linear algebraic matrix equation to solve for the coefficients a_{ik}	$\begin{pmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 2 & 0 & 0 & 0 \\ 1 & \tau_f & \tau_f^2 & \tau_f^3 & \tau_f^4 & \tau_f^5 \\ 0 & 1 & 2\tau_f & 3\tau_f^2 & 4\tau_f^3 & 5\tau_f^4 \\ 0 & 0 & 2 & 6\tau_f & 12\tau_f^2 & 20\tau_f^3 \end{pmatrix} \begin{pmatrix} a_{i0} \\ a_{i1} \\ a_{i2} \\ a_{i3} \\ a_{i4} \\ a_{i5} \end{pmatrix} = \begin{pmatrix} x_{i0} \\ x'_{i0} \\ x''_{i0} \\ x_{if} \\ x'_{if} \\ x''_{if} \end{pmatrix}$	$\begin{pmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 2 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 6 & 0 & 0 & 0 \\ 1 & \tau_f & \tau_f^2 & \tau_f^3 & \tau_f^4 & \tau_f^5 & \tau_f^6 \\ 0 & 1 & 2\tau_f & 3\tau_f^2 & 4\tau_f^3 & 5\tau_f^4 & 6\tau_f^5 \\ 0 & 0 & 2 & 6\tau_f & 12\tau_f^2 & 20\tau_f^3 & 30\tau_f^4 \end{pmatrix} \begin{pmatrix} a_{i0} \\ a_{i1} \\ a_{i2} \\ a_{i3} \\ a_{i4} \\ a_{i5} \\ a_{i6} \end{pmatrix} = \begin{pmatrix} x_{i0} \\ x'_{i0} \\ x''_{i0} \\ x''_{i0} \\ x_{if} \\ x'_{if} \\ x''_{if} \end{pmatrix}$				



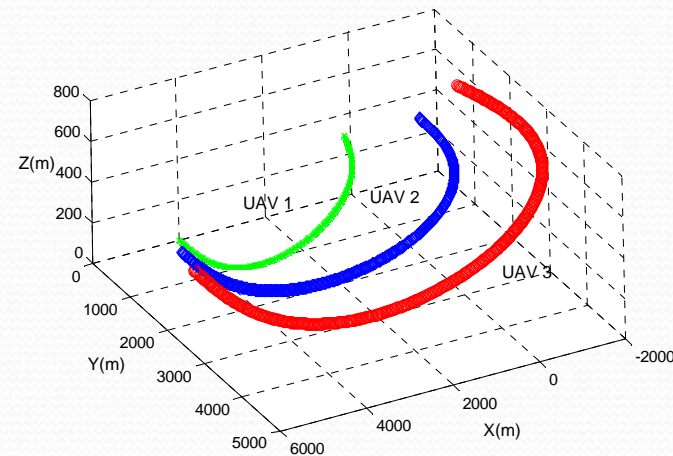
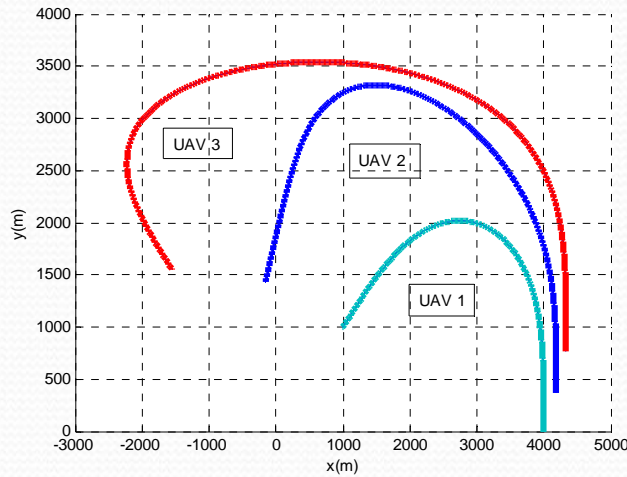
Impact of changing total path length



Impact of changing total path length and initial jerk

Imp Critical Coordination: RT Path Planning

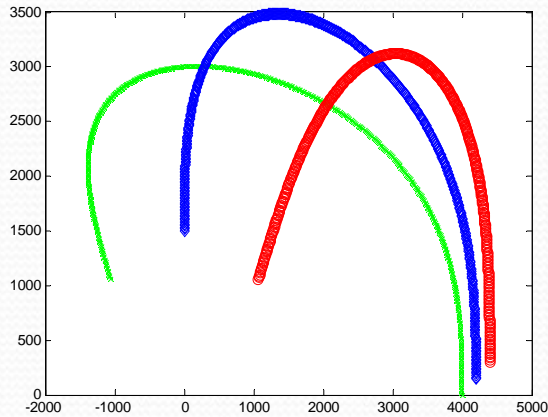
- Deconfliction in space – sequentially assigned final conditions



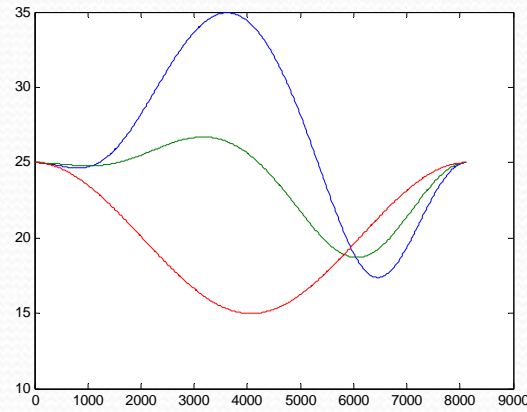
- essentially a 2D solution

t_{fl}	dt	AM	v_{min}	v_1	v_2	v_3	v_{max}	d_{min}
235s	.005s	48s	15 m/s	16m/s	21m/s	30.2m/s	35m/s	203m

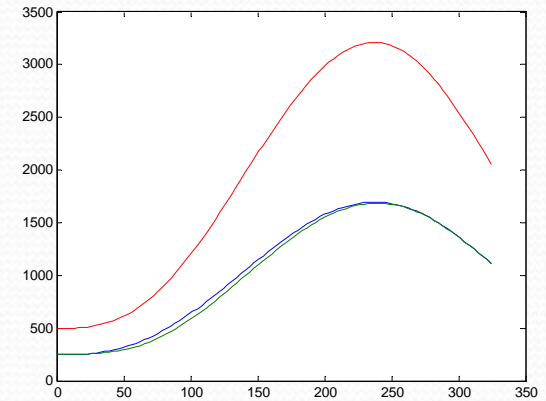
- Multiple UAVs – simultaneous arrival (deconfliction in time)



3D paths



Speed profiles



distances

$$t_f = 324 \text{ sec}, AM = 271 \text{ sec}$$

In this case the paths intersect, but if each vehicle follows the nominal speed profile they will maintain a minimum separation distance at all times – disturbance rejection is addressed at the **coordination level**

UAV Path Following Concept

- ❑ **Objective:** follow predefined spatial 3D paths
 - paths are time-independent:
 - decoupling between space and time = separation of 3D path and speed
 - speed can be used as an additional DOF for time coordination
- ❑ **Limitation:** Traditional UAV AP is not designed to follow an aggressive 3D path.
- ❑ **Solution:** Adaptive augmentation without any modifications to commercial autopilot
 - Conventional solution – backstepping – requires modification of source code of A/P
 - Global results – but cancels inner loop

Intuitive Analogy

Analogous to “Tunnel in the Sky” concept familiar to pilots of 3D path and speed profile following

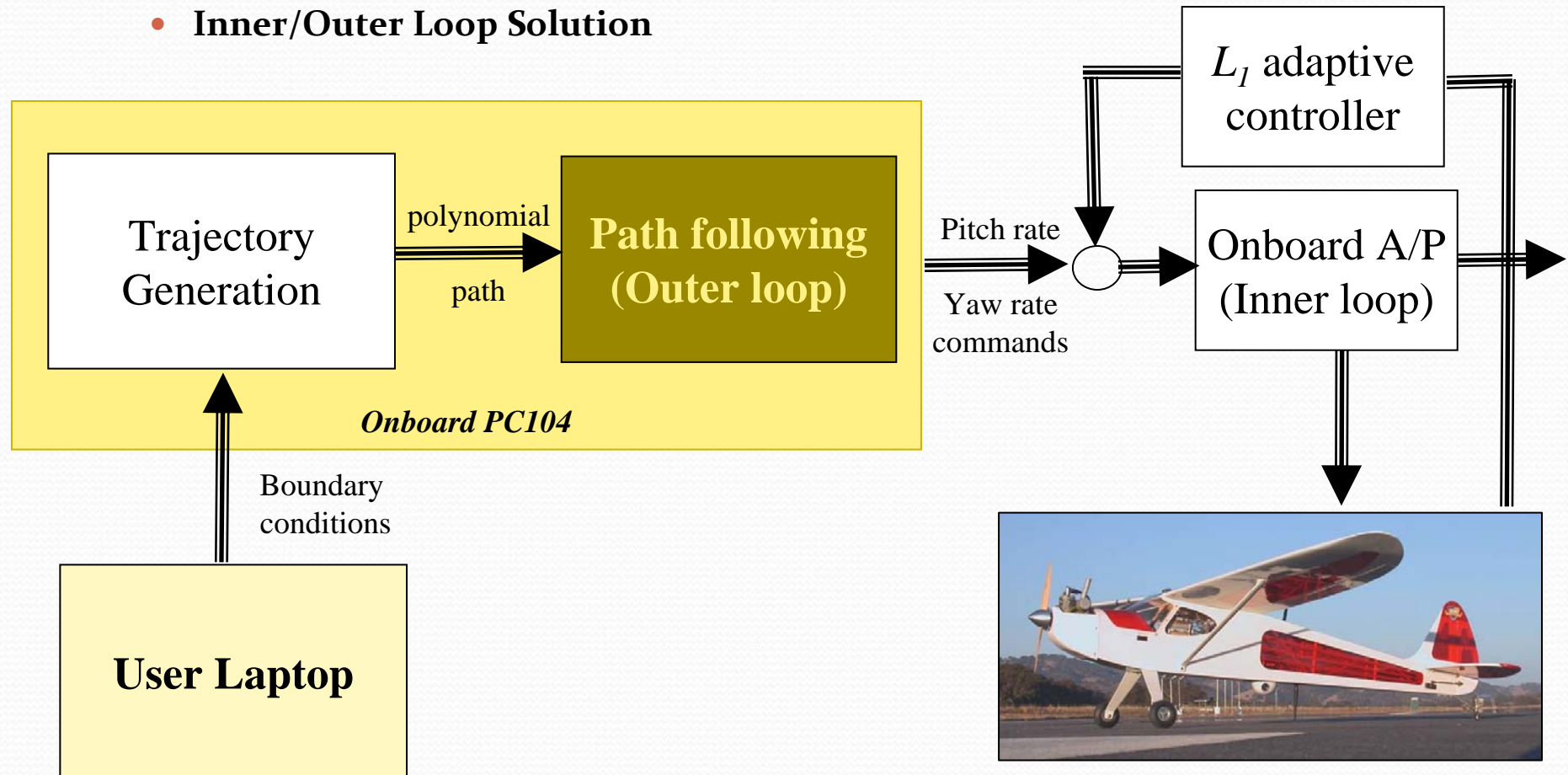


Eliminate path following (both distance and attitude) errors using angular rates

Follow speed profile to keep the a/c within its dynamic limitations.

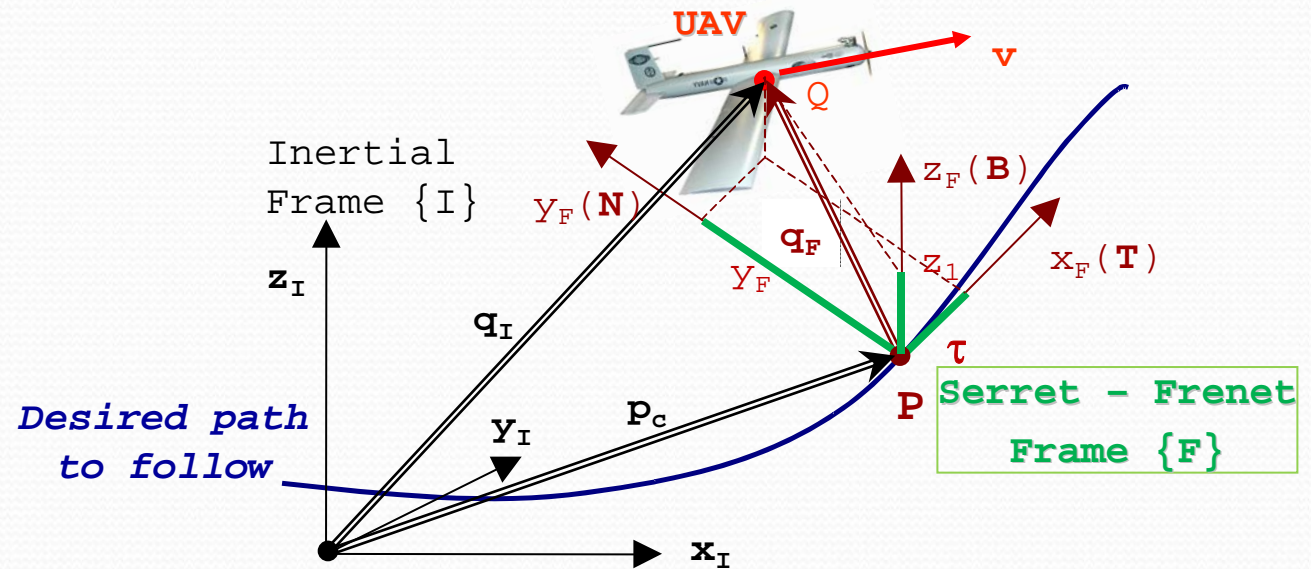
UAV Path Following

- System Architecture
 - Inner/Outer Loop Solution



Problem Geometry

- ❑ **F: Serret-Frenet frame**
- ❑ **W: wind frame**
- ❑ **I: inertial frame**
- ❑ $p_c(l)$ desired trajectory
- ❑ $v(t)$ UAV speed
- ❑ γ flight path angle
- ❑ ψ heading angle
- ❑ τ path length
- ❑ $q_I = [x_I \ y_I \ z_I]$ position of UAV in inertial frame



3D Kinematics Equations

$$\begin{aligned} dx_I / dt &= v \cos \gamma \cos \psi \\ dy_I / dt &= -v \cos \gamma \sin \psi \\ dz_I / dt &= v \sin \psi \end{aligned}$$

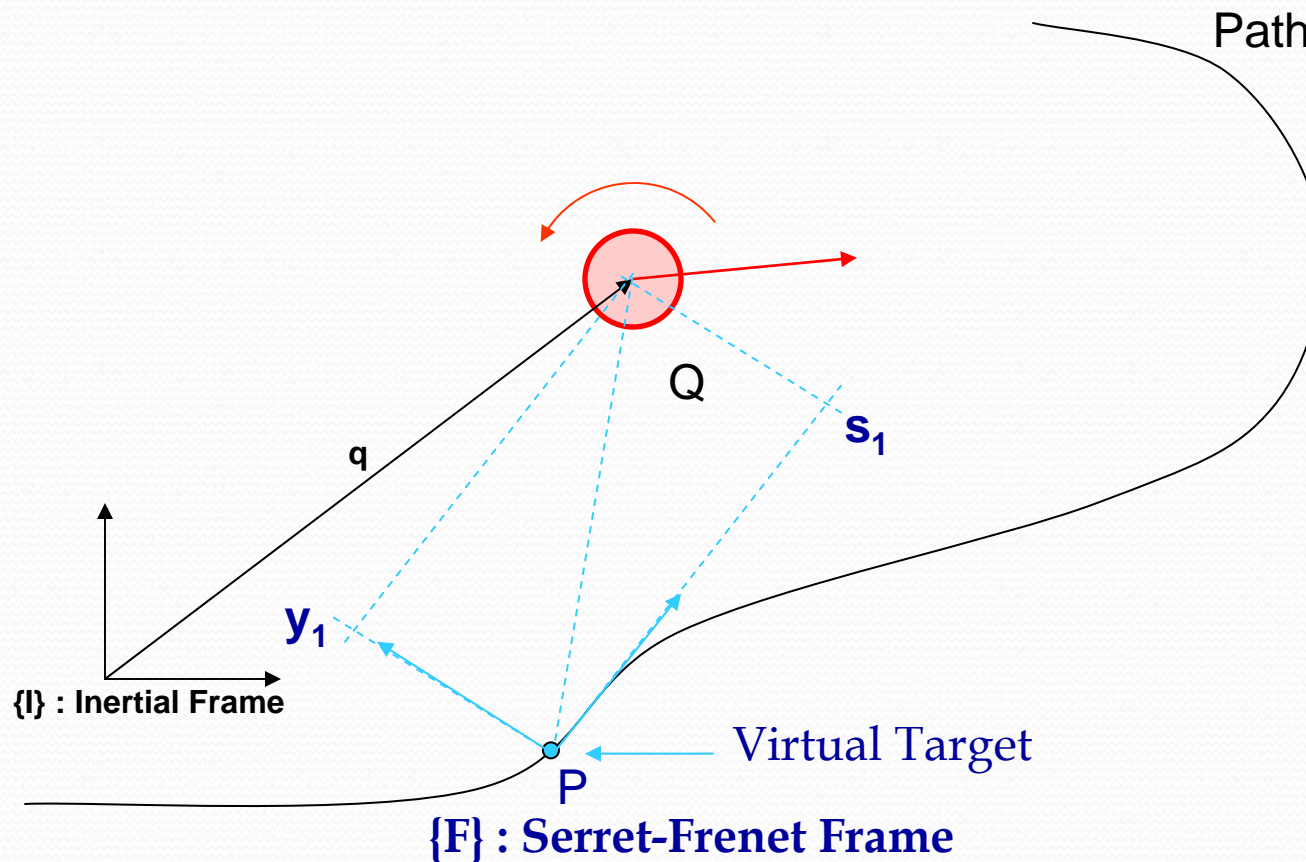
$$\begin{bmatrix} d\gamma / dt \\ d\psi / dt \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & \cos^{-1} \gamma \end{bmatrix} \begin{bmatrix} q \\ r \end{bmatrix}$$

$$d\tau / dt = \tau_v$$

Input: q
 r
 τ_v

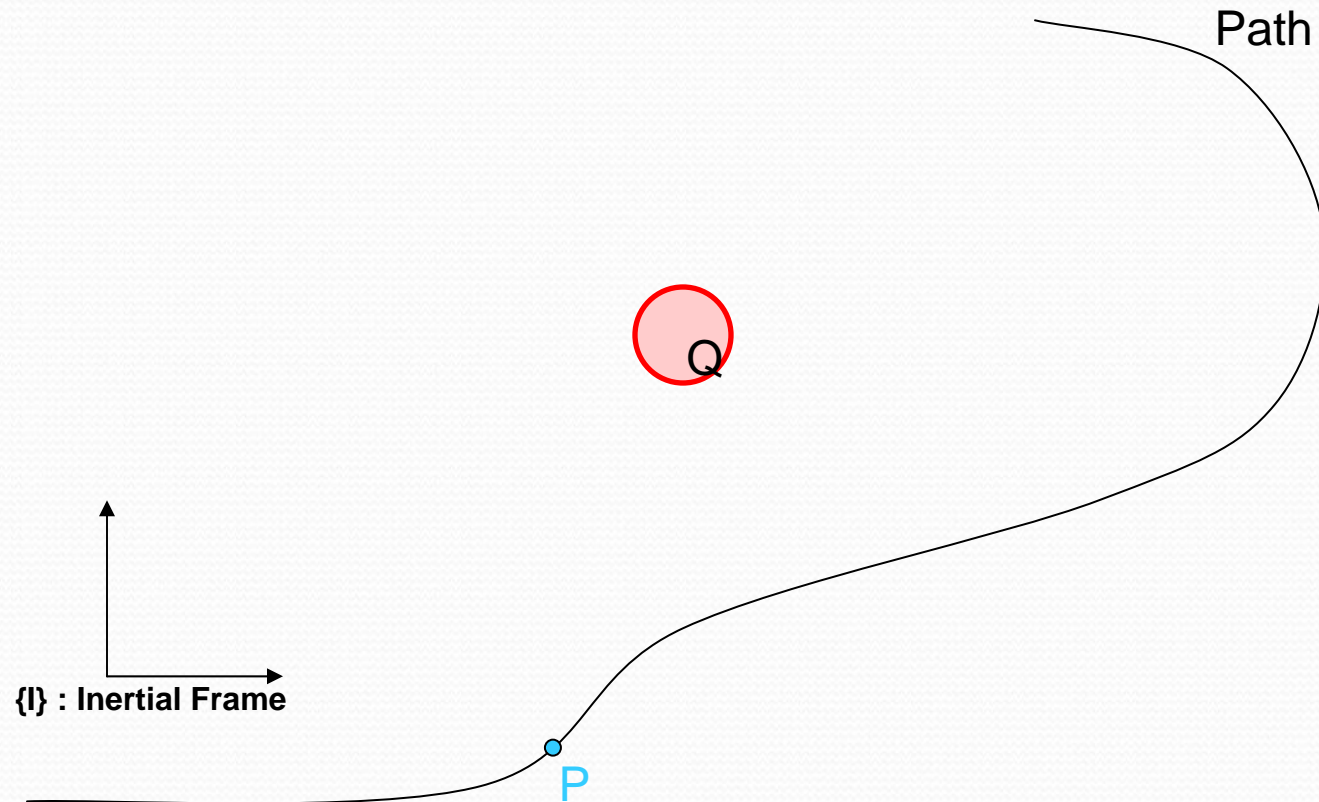
UAV Path Following

- ❑ **Key idea:** use virtual target to determine desired location on the path
 - Minimize the distance from the UAV to the virtual target on the path
 - Reduce the angle between the vehicle velocity vector and local tangent to the path
- ❑ Virtual target's motion – *extra degree of freedom*



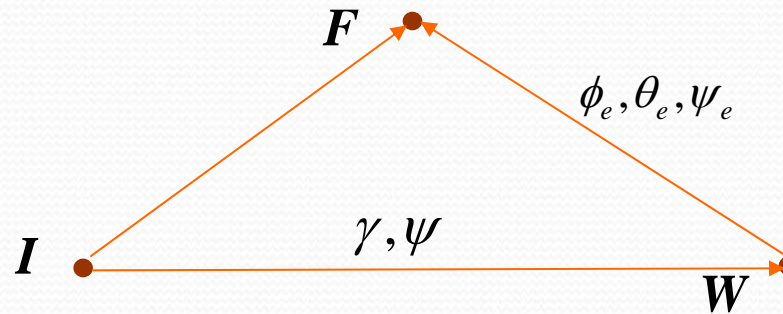
UAV Path Following (cont.)

Control the evolution of the virtual target : added degree of freedom



Kinematics

Coordinate systems



$$q_F = [x_F \ y_F \ z_F]$$

- difference between q_I and $p_c(\tau)$ in F

$$\phi_e, \theta_e, \psi_e$$

- Euler angles from F to W

Kinematics equations in I

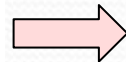
$$\dot{x}_I = v \cos \gamma \cos \psi$$

$$\dot{y}_I = -v \cos \gamma \sin \psi$$

$$\dot{z}_I = v \sin \gamma$$

$$\begin{bmatrix} \dot{\gamma} \\ \dot{\psi} \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & \cos^{-1} \gamma \end{bmatrix} \begin{bmatrix} q \\ r \end{bmatrix}$$

$$\dot{\tau} = \tau_v$$



Error Equations in F

$$G_e := \begin{cases} dx_F / dt = -\tau_v (1 - \kappa(\tau) y_F) + v \cos \theta_e \cos \psi_e \\ dy_F / dt = -\tau_v (\kappa(\tau) x_F - \zeta(\tau) z_F) + v \cos \theta_e \sin \psi_e \\ dz_F / dt = -\zeta(\tau) \tau_v y_F - v \sin \theta_e \\ \begin{bmatrix} d\theta_e / dt \\ d\psi_e / dt \end{bmatrix} = D(t, \theta_e, \psi_e) + T(t, \theta_e) \begin{bmatrix} q \\ r \end{bmatrix} \\ d\tau / dt = \tau_v \end{cases}$$

where

ζ - torsion

κ - curvature

Kinematic Control Law

$$V_c = \frac{1}{2c_1} (x_F^2 + y_F^2 + z_F^2) + \frac{1}{2c_2} (\theta_e - \delta_\theta)^2 + \frac{1}{2c_3} (\psi_e - \delta_\psi)^2$$

Desired shaping functions $\delta_\theta(t) = \sin^{-1} \left(\frac{z_F(t)}{|z_F(t)| + d_1} \right)$, $\delta_\psi(t) = \sin^{-1} \left(\frac{y_F(t)}{|y_F(t)| + d_2} \right)$

$$\begin{bmatrix} q_c \\ r_c \end{bmatrix} = T^{-1}(t, \theta_e) \left(\begin{bmatrix} u_{\theta_c} \\ u_{\psi_c} \end{bmatrix} - D(t, \theta_e, \psi_e) \right)$$

Path following control laws

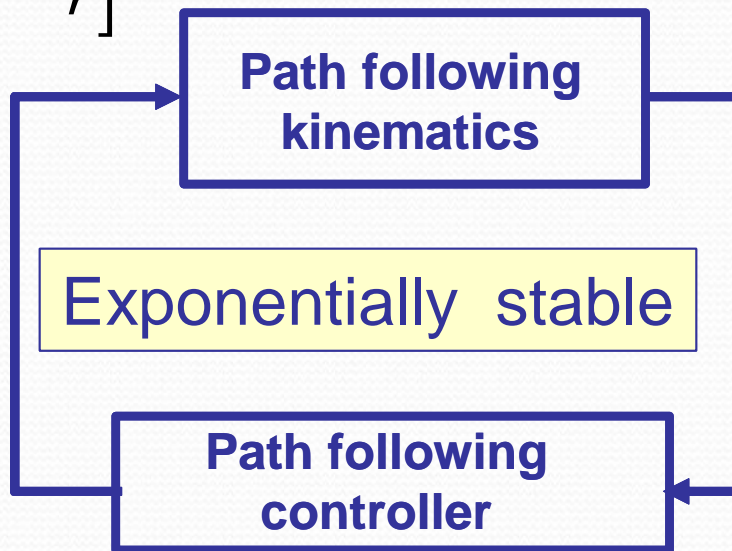
$$\dot{t} = K_1 x_F + v \cos \theta_e \cos \psi_e$$

$$u_{\theta_c} = -K_2 (\theta_e - \delta_\theta) + \frac{c_2}{c_1} z_F v \frac{\sin \theta_e - \sin \delta_\theta}{\theta_e - \delta_\theta} + \dot{\delta}_\theta$$

$$u_{\psi_c} = -K_3 (\psi_e - \delta_\psi) - \frac{c_2}{c_1} y_F v \cos \theta_e \frac{\sin \psi_e - \sin \delta_\psi}{\psi_e - \delta_\psi} + \dot{\delta}_\psi$$

Kinematic Control Law

$$y = [q \quad r]^T$$

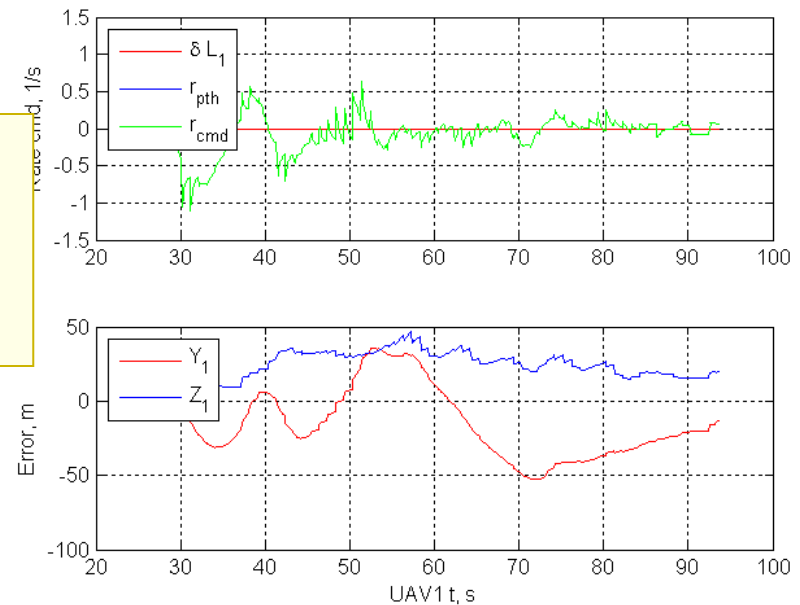
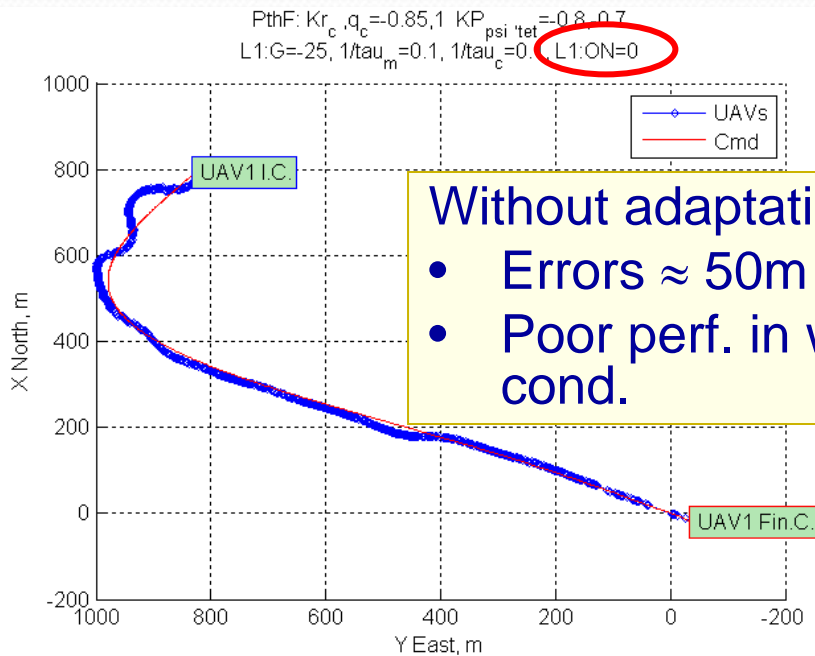
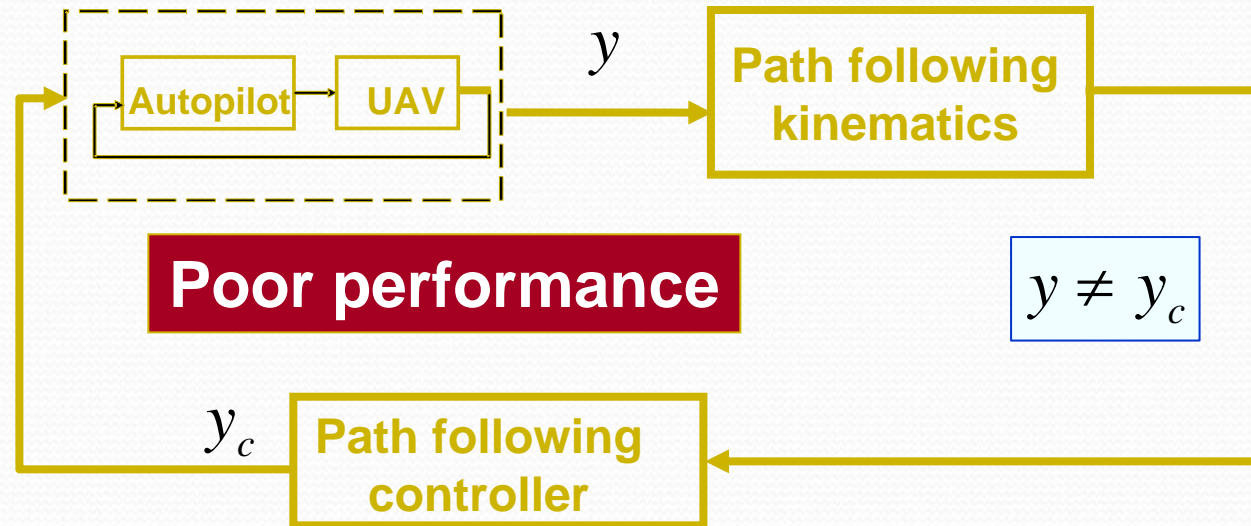


$$\dot{V}_c \leq -\alpha V_c$$

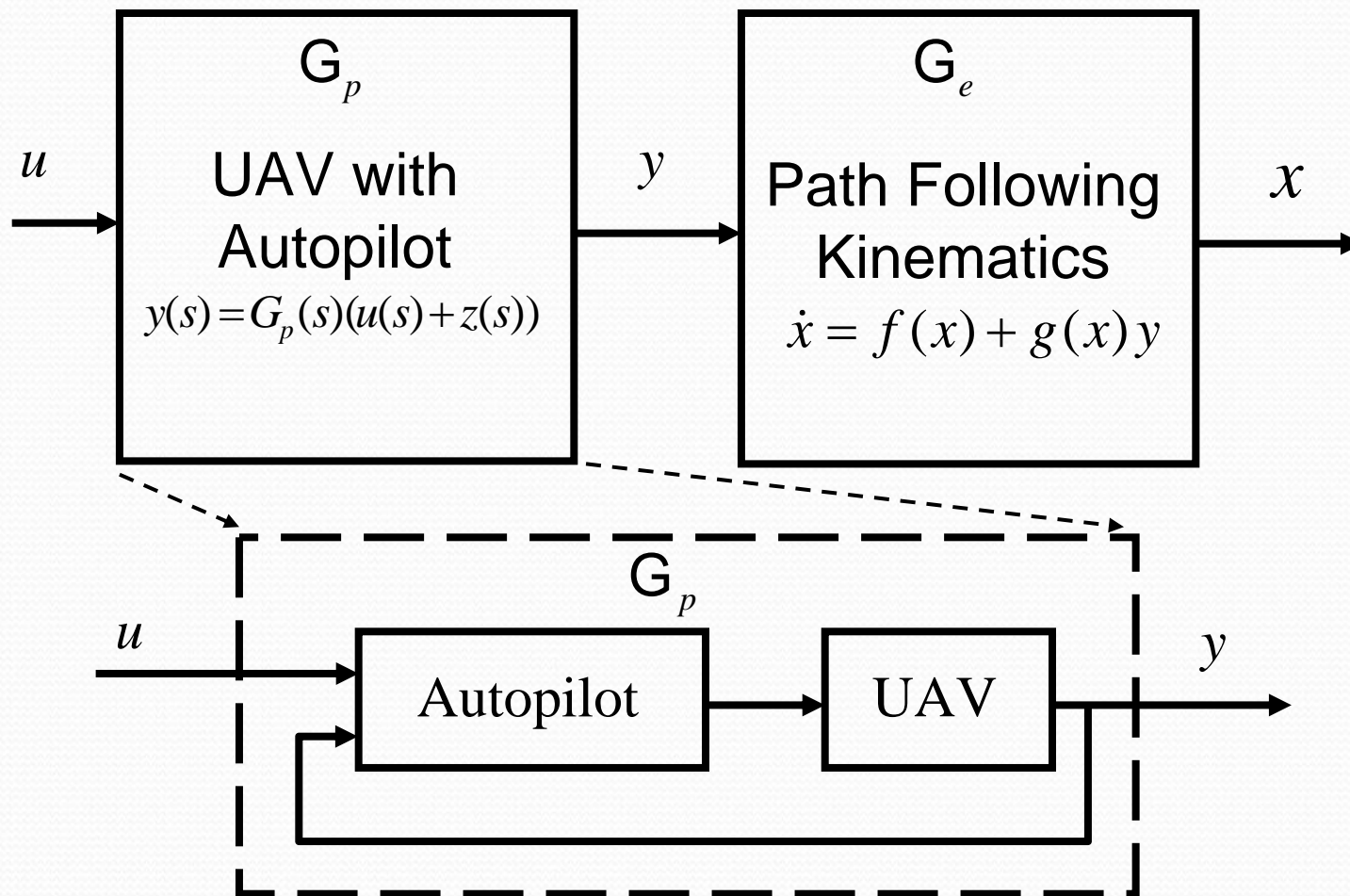
Semiglobal result:
true for all kinematic error states
initialized in arbitrary region Ω

$$y_c = [q_c \quad r_c]^T$$

Degradation of Performance



Cascaded System



- ❑ Conventional solution – backstepping – requires modification of source code of A/P
- ❑ Global results – but cancels inner loop

Problem Reformulation

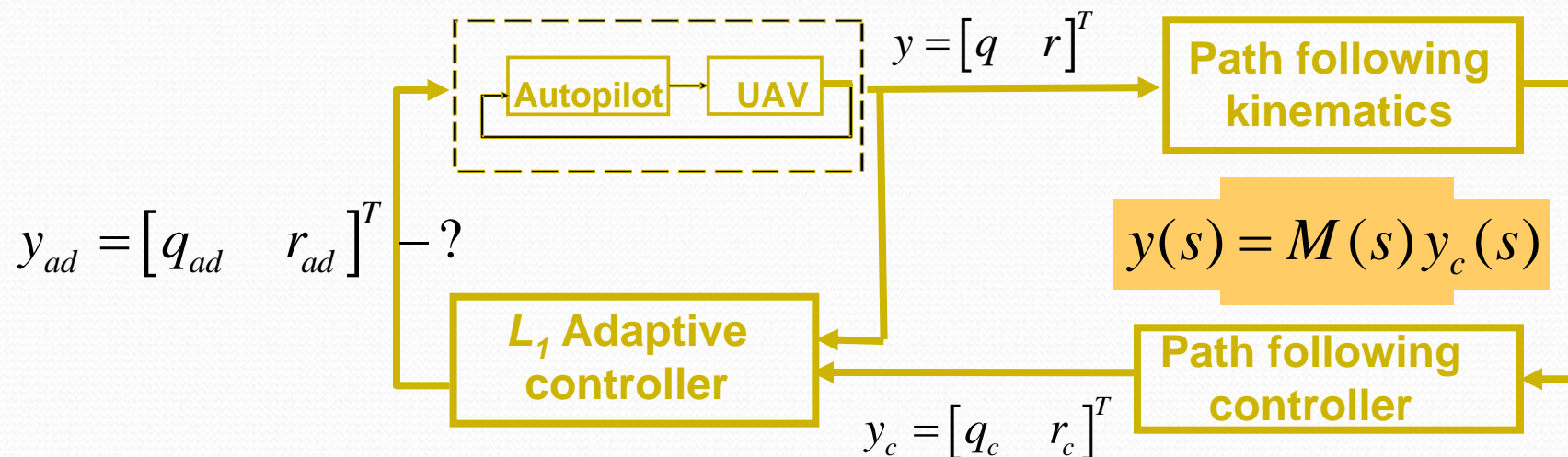
UAV with autopilot $q(s) = G_q(s) (q_c(s) + z_q(s))$

$r(s) = G_r(s) (r_c(s) + z_r(s))$

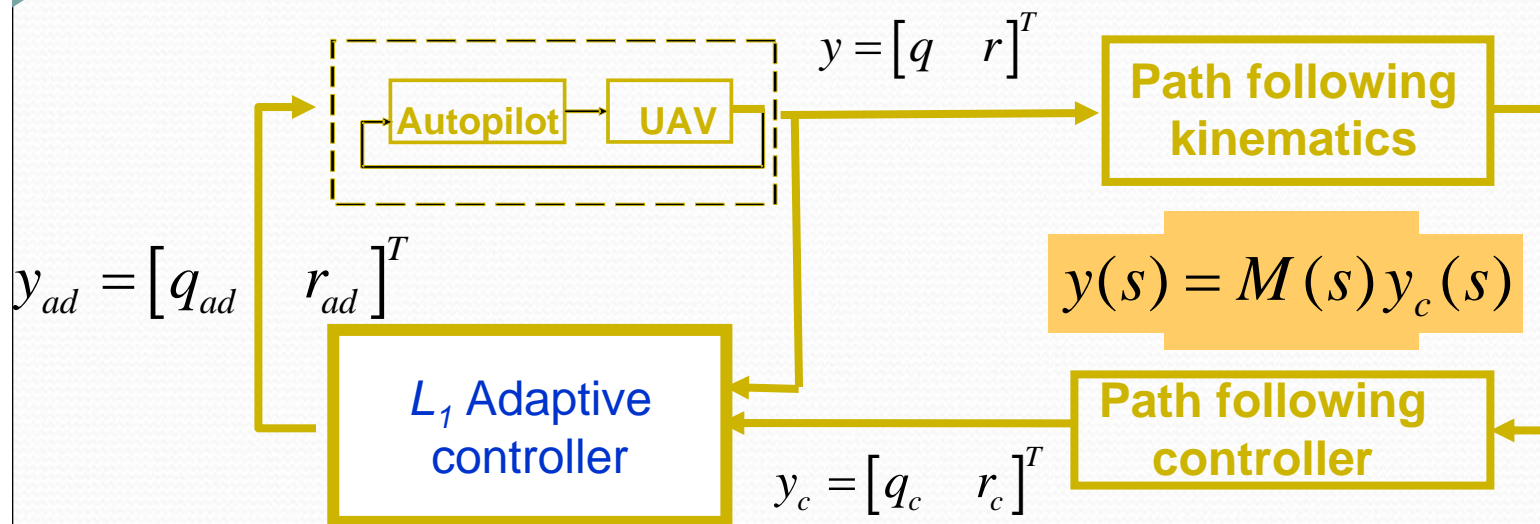
Design objective $q(s) \approx M(s) q_c(s)$

$r(s) \approx M(s) r_c(s)$

$$M(s) = \frac{m}{s+m}$$



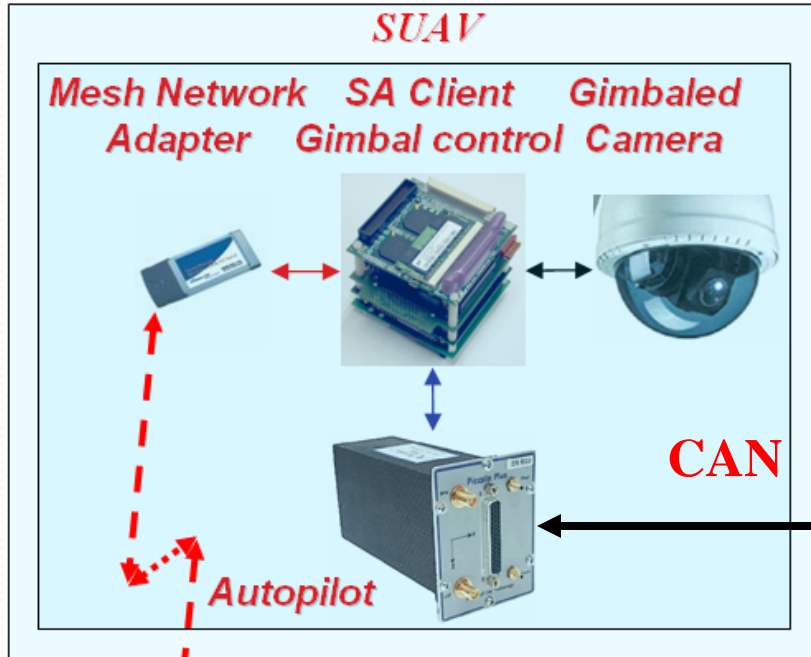
Path Following: Summary



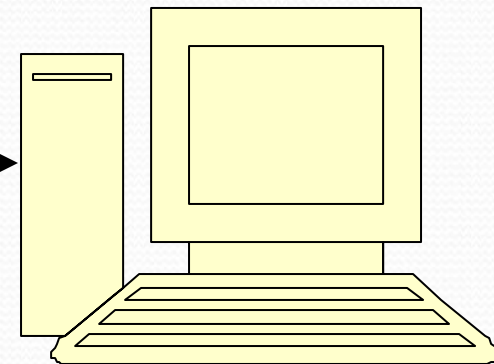
- ❑ The cascaded system is UUB
- ❑ The UUB can be reduced via selection of the filter bandwidth and the reference system bandwidth
 - ➔ Reducing the UUB leads to reduced robustness
- **L1 guarantees that the region of attraction for kinematic errors does not change**

Hardware-in-the-Loop Simulation

Airborne Segment



Ground Segment

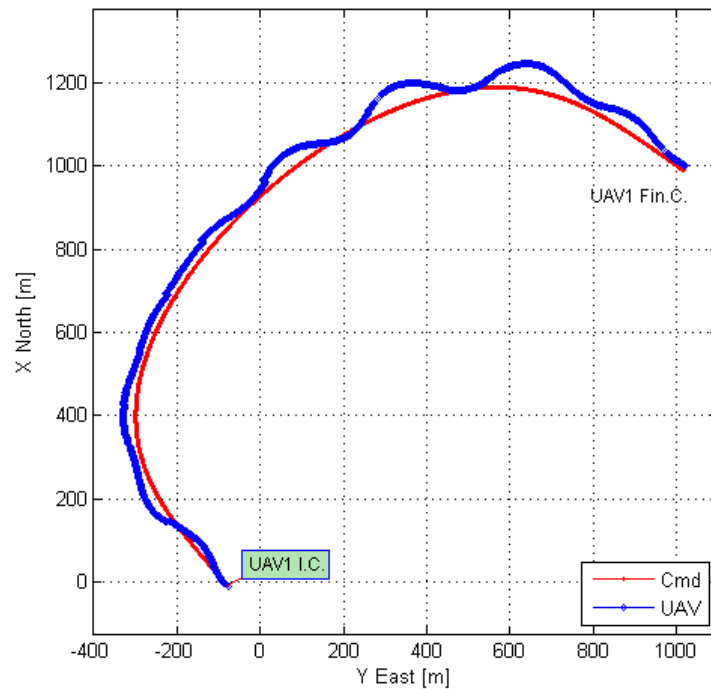


**6DOF nonlinear
model of the UAV**

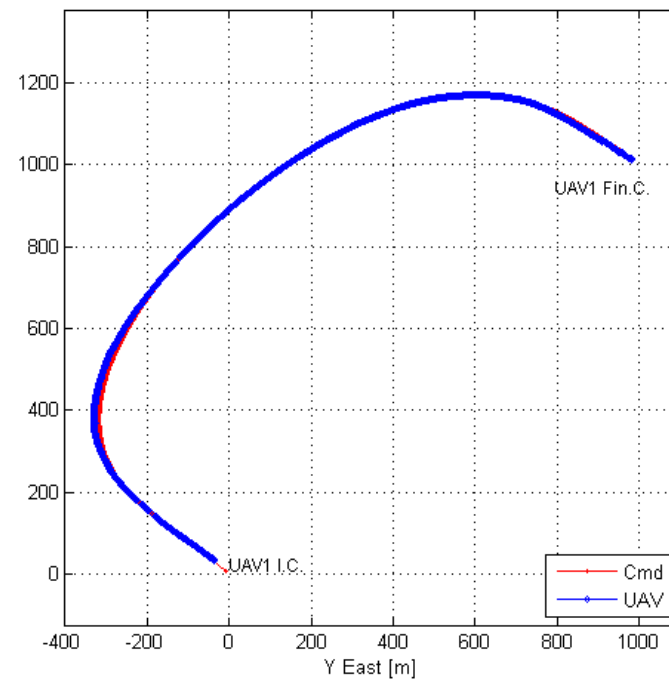
Hardware-in-the-Loop Simulation

- comparison: with and without adaptation

Path following
w/o L_1 adaptation



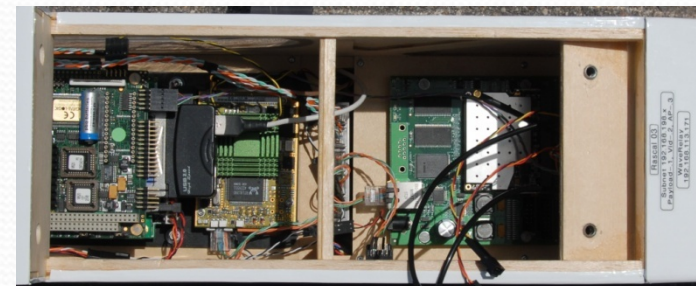
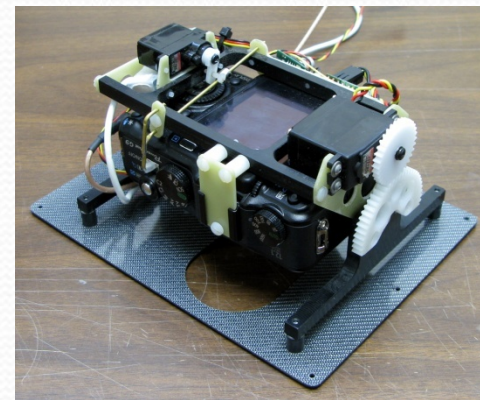
Path following
with L_1 adaptation



Hardware (Second Generation)

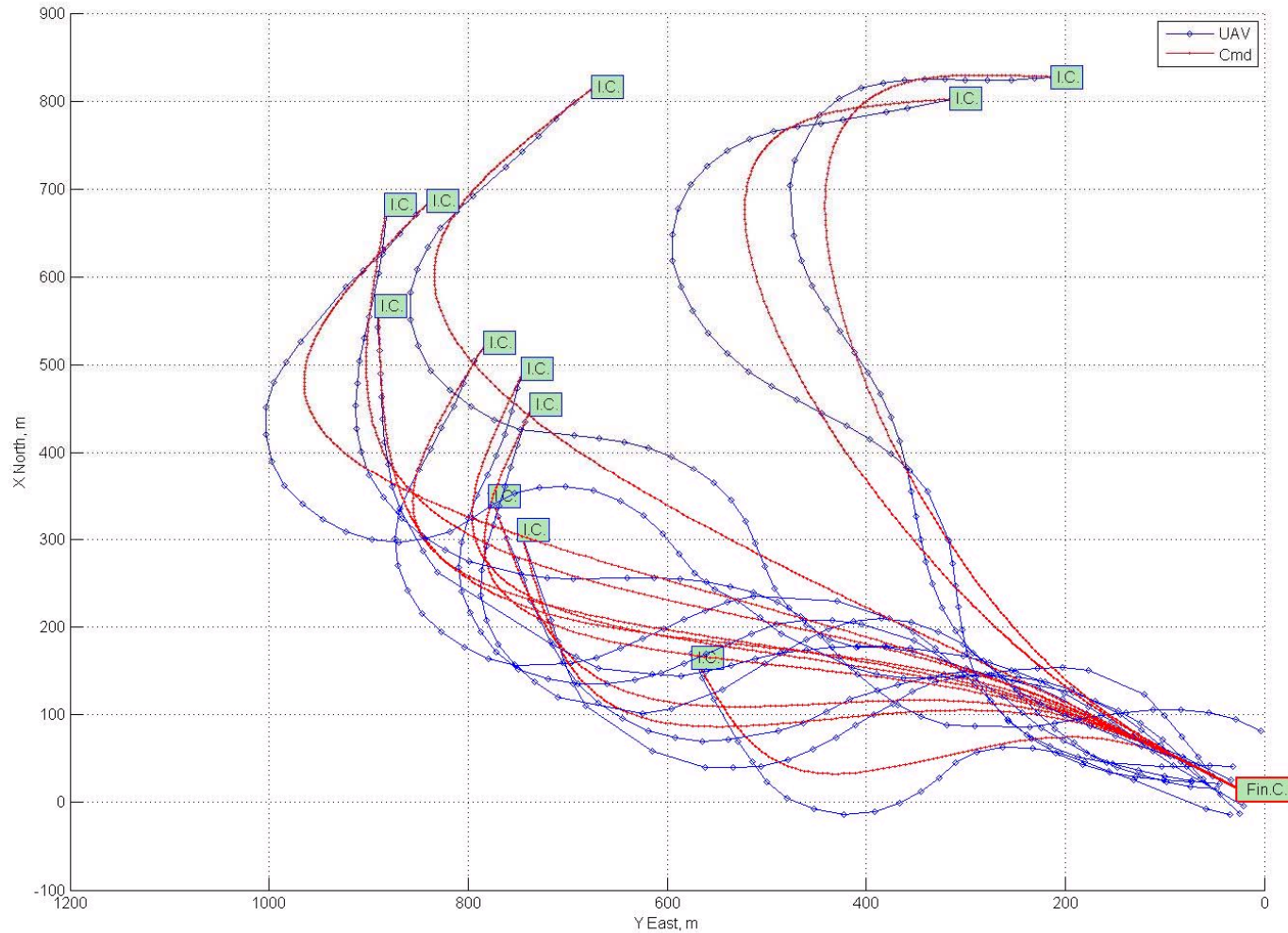
● Networked Aircraft

- Airframe; Sig Rascal 110
 - 2.8 meter span, 8 kg
 - 26 cc gas engine
 - 2-3 hour endurance
 - 15-35 m/s velocity
- Payload:
 - Cannon G9 12Mp gimbaled Camera
 - PC104 with Wave Relay Mesh card
 - PC104 for gimbal control and AP interface
 - ADL MSMT₃SEG
 - PELCO-NET 350 video server



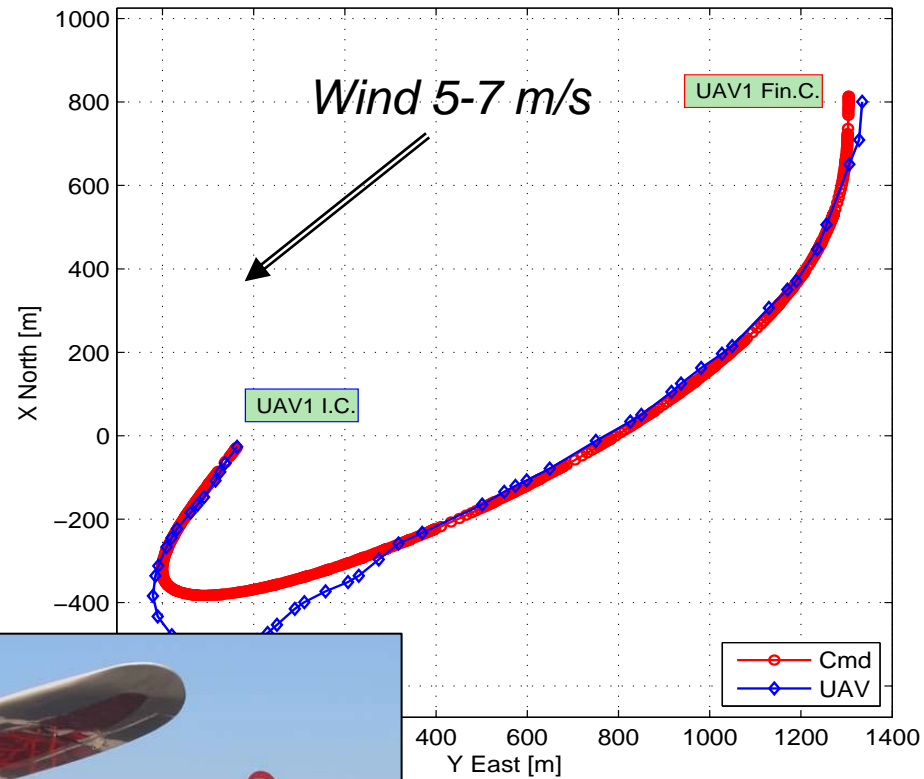
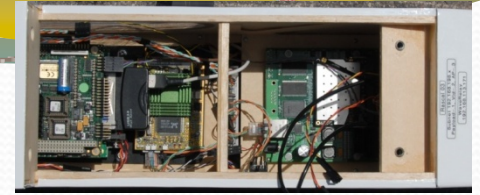
Flight Test Results: Path Following

- no adaptation – effect of gain changes



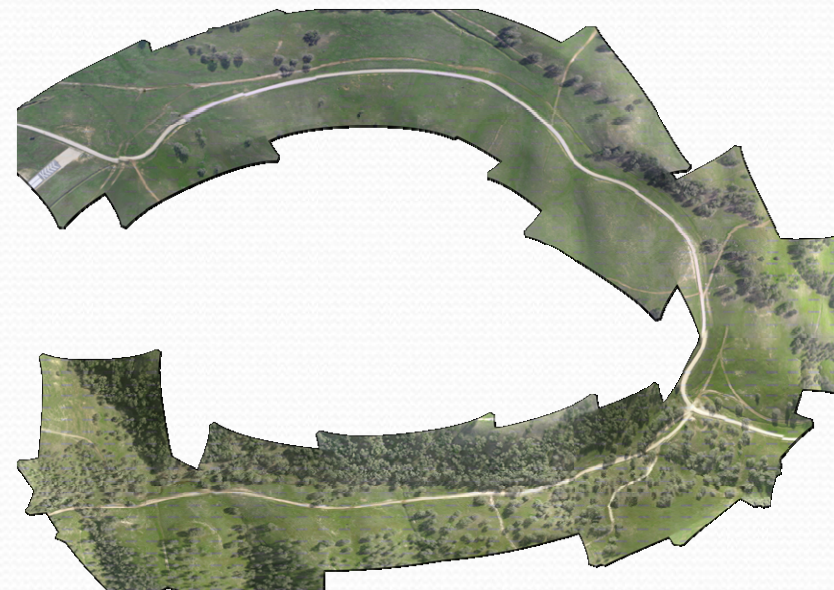
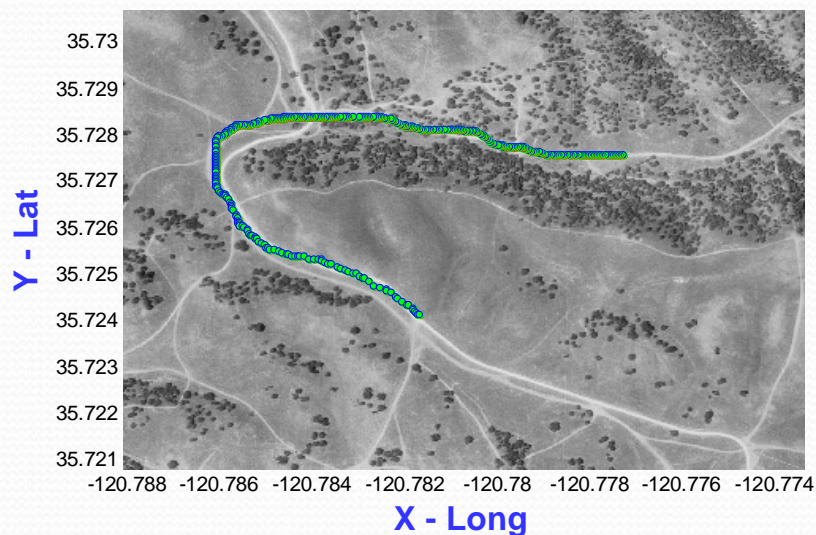
Flight Test Results: Path Following

L1 ON



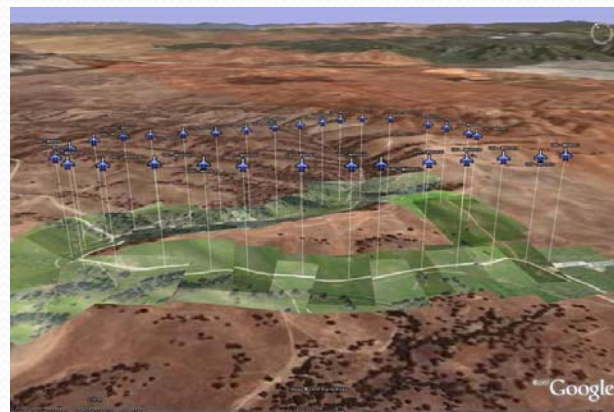
Feature Following using Path Following

Desired Trajectory Generation



Resulting Mosaic using Overlaid G9 images

Feature Selection



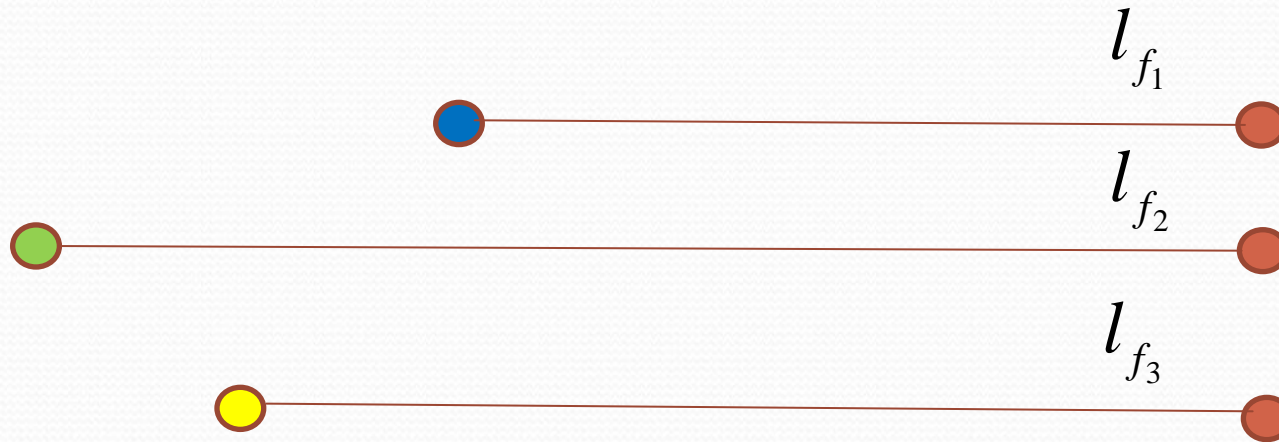
Google Earth Overlay

Time-Critical Coordinated Motion Control



*UAVs must arrive at the same time;
absolute time is not a priority!*

Time-Critical Coordinated Motion Control



Paths parameterized by length ($\tau=l$)

l_{f_i} - length of path for vehicle i

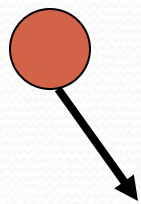
t_f - time of arrival (unknown)

$$l'_{f_i}(t) = l_i(t) / l_{f_i}; l'_{f_i}(t_f) = 1, \forall i$$

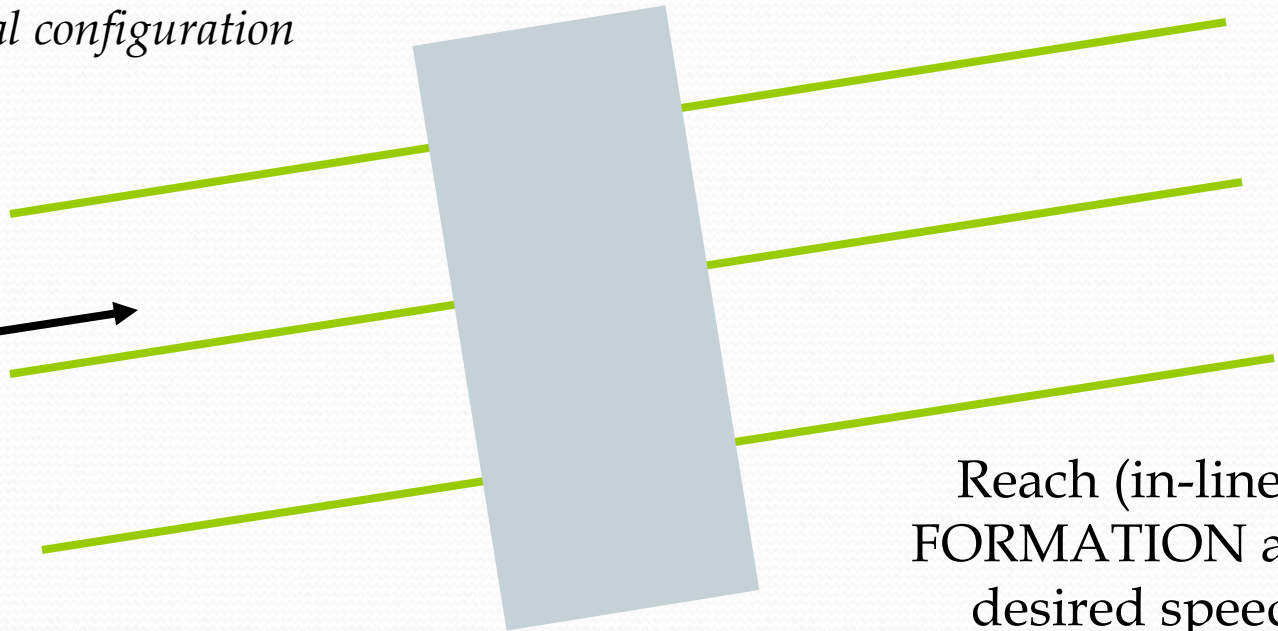
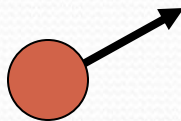


Coordinated Path Following

PATHS (HIGHWAYS TO BE FOLLOWED)



Initial configuration



Reach (in-line)
FORMATION at a
desired speed

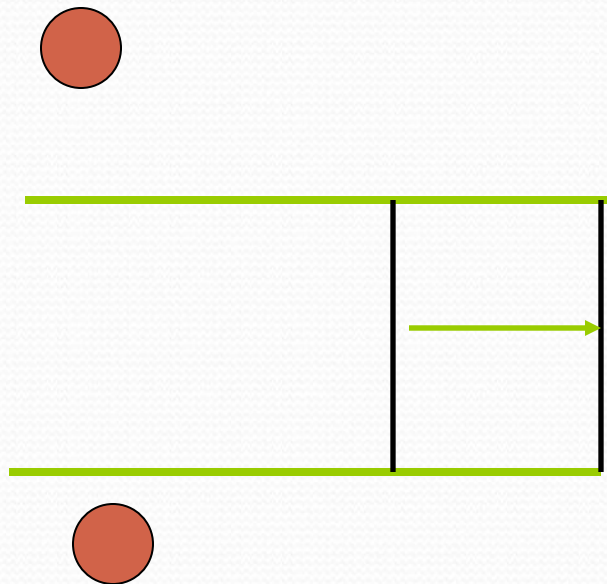
v_d !

IN-LINE FORMATION

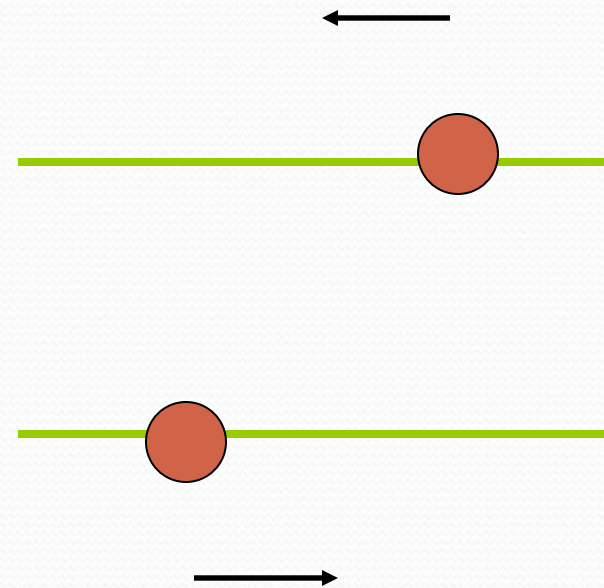
Divide to Conquer Approach

*Each vehicle runs its own
PATH FOLLOWING
controller to steer itself to the path*

*Vehicles TALK and adjust their
SPEEDS in order to COORDINATE
themselves (reach formation)*

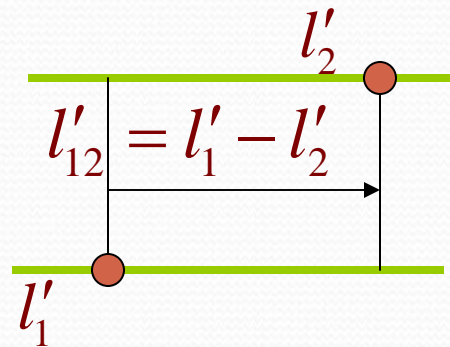


Coordination error

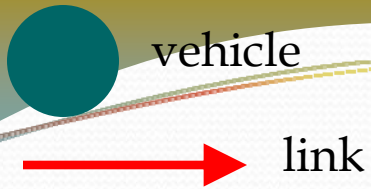


Coordination state / error

Coordination error
(in-line formation): l'_{12}

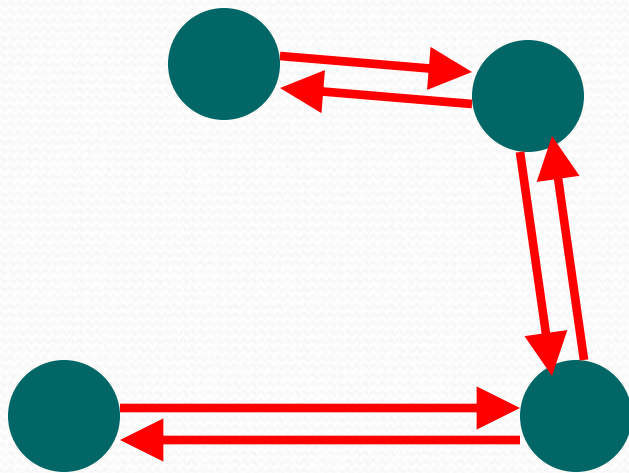


Normalized Path lengths l'_1 and l'_2

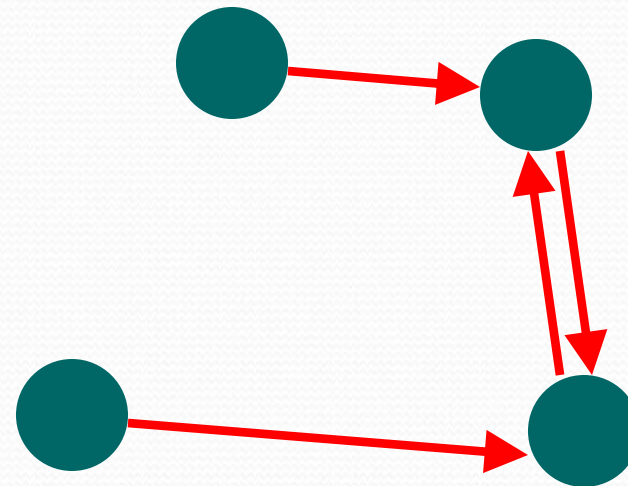


Communication Constraints

What is the communications topology? (**GRAPH**)



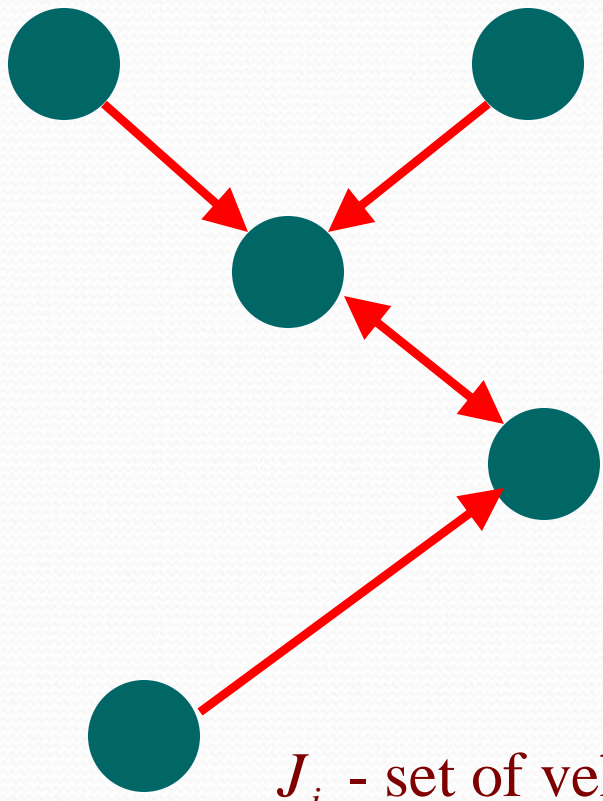
Bidirectional Links
→ *undirected graphs*



Non-bidirectional links
→ *directed graphs*

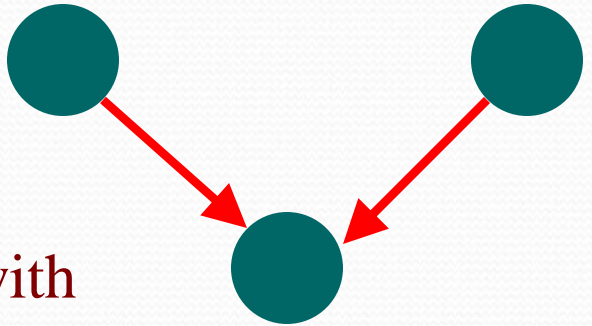
R. Murray [2002], B. Francis [2003], A. Jadbabaie [2003]

Communication Constraints



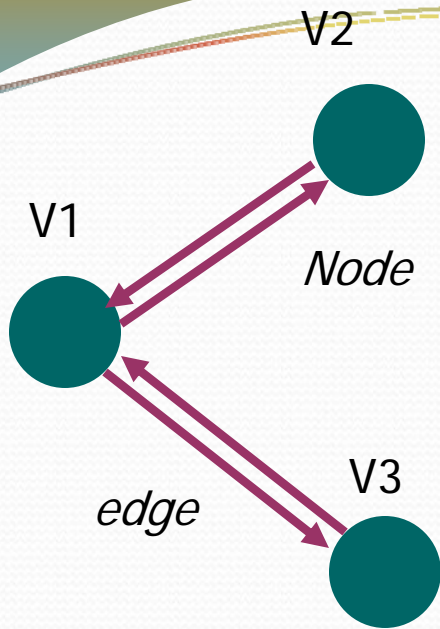
- Communication Delays*
- Temporary Loss of Comms*
- Switching Comms Topology*
- Asynchronous Comms*

J_i - set of vehicles that vehicle i communicates with



Links with Networked Control and Estimation Theory

Communication Constraints



Adjacency
Matrix A

$$= \begin{bmatrix} 0 & 1 & 1 \\ 1 & 0 & 0 \\ 1 & 0 & 0 \end{bmatrix}$$

Degree
Matrix D

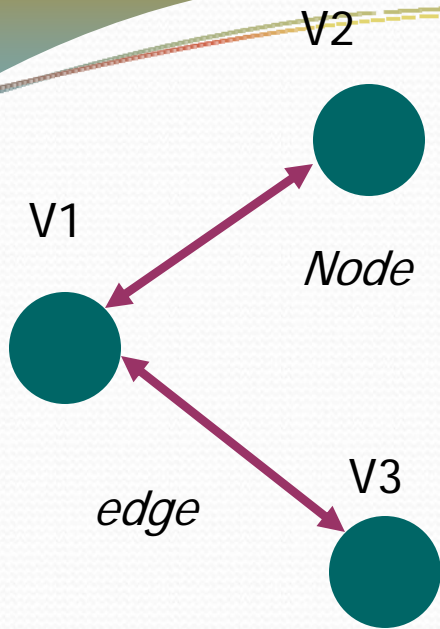
$$= \begin{bmatrix} 2 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

V1 receives info from *neighbours* V2 and V3

V2 receives info from *neighbour* V1

V3 receives info from *neighbour* V1

Communication Constraints



Laplacian

$$L = D - A = \begin{pmatrix} 2 & -1 & -1 \\ -1 & 1 & 0 \\ -1 & 0 & 1 \end{pmatrix}$$

$$L \begin{pmatrix} l'_1 \\ l'_2 \\ l'_3 \end{pmatrix} = \begin{pmatrix} (l'_1 - l'_2) + (l'_1 - l'_3) \\ l'_2 - l'_1 \\ l'_3 - l'_1 \end{pmatrix}$$

Neighbour set 1 = { V2 , V3 }

Neighbour set 2 = { V1 }

Neighbour set 3 = { V1 }

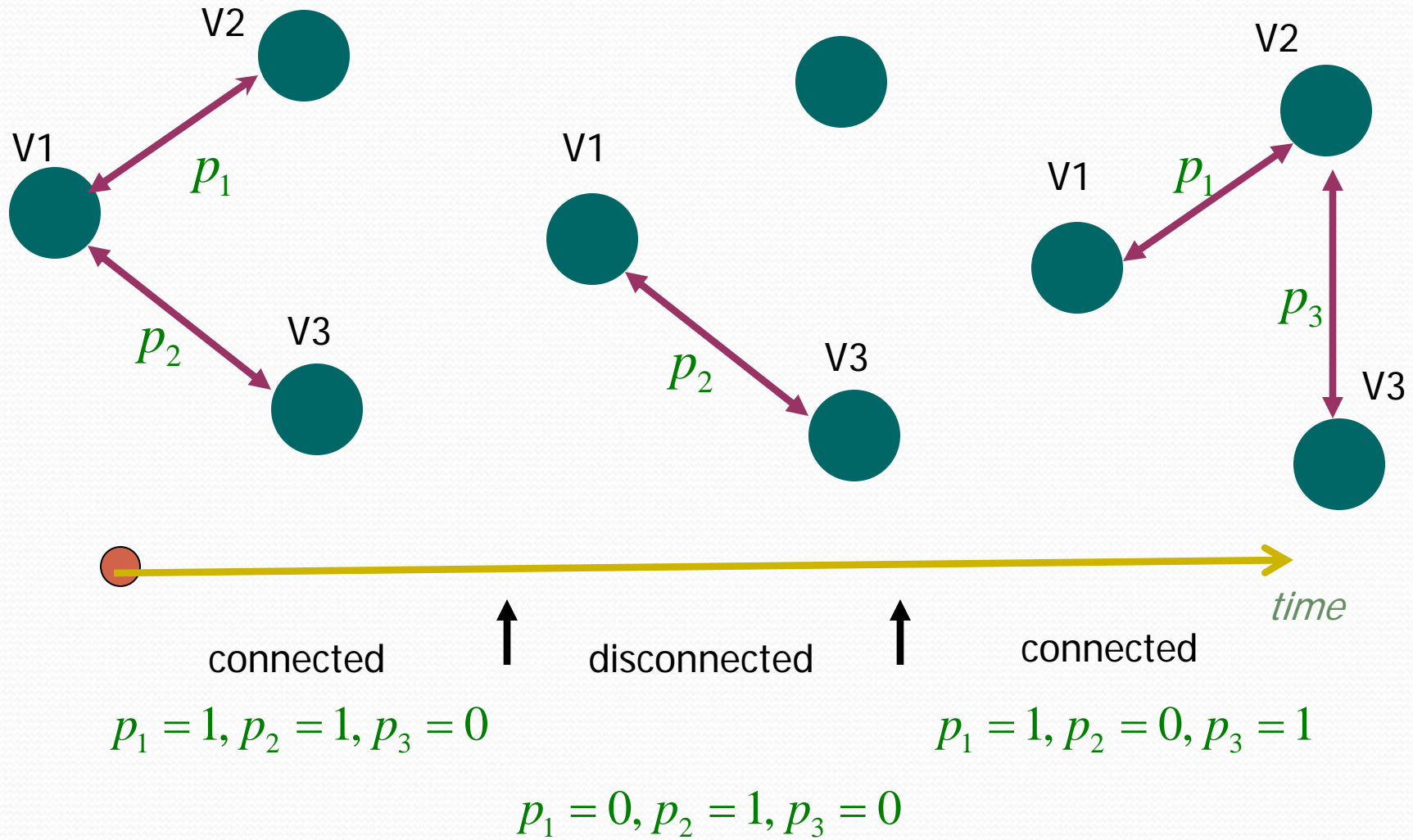
Properties:

- $L1 = 0$

- Graph is connected $\Rightarrow \text{rank} L = n - 1 = 2$

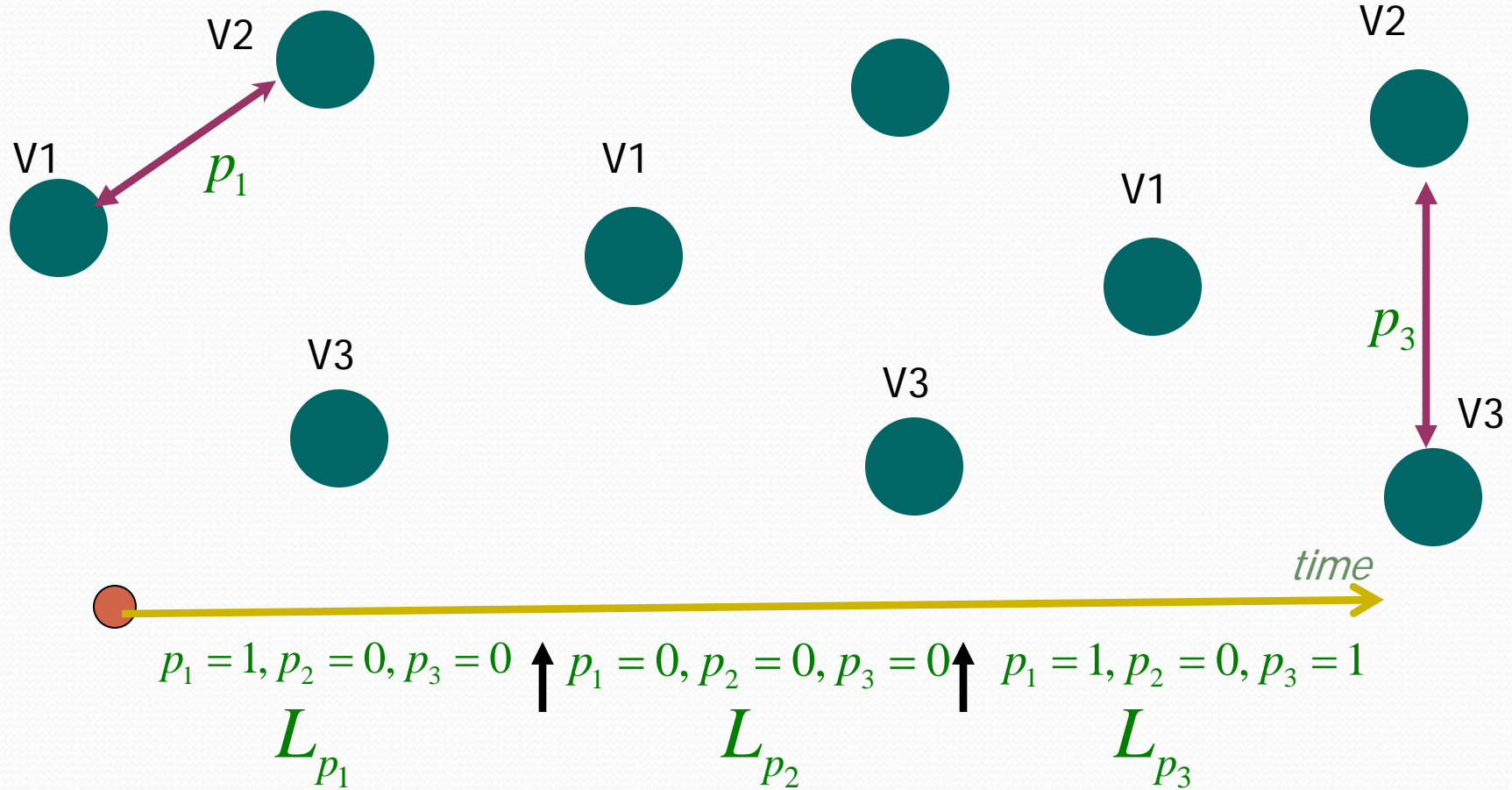
$$Ll' = 0 \Rightarrow l'_1 = l'_2 = l'_3$$

Switching Communications: brief connectivity losses



L is a function of p , denoted L_p

Switching Communications: “uniformly” connected in mean



the union graph over
time interval T
is connected

$$L_{[t,t+T]} = L_{p_1} + L_{p_2} + L_{p_3}$$

$$\Rightarrow \begin{cases} \text{rank } L_{[t,t+T]} = n - 1 = 2 \\ L_{[t,t+T]} \mathbf{1} = 0 \end{cases}$$

Time-Critical Coordinated Motion Control

Coordination Control Law

$$dl_i / dt = \kappa_1 x_{Fi} + v_i \cos \theta_{e,i} \cos \psi_{e,i}$$

Remember from Path Following



Adjust at the Coordination Level!

$$v_{c_i} = \frac{u_{\text{coord}_i} l_{fi} - \kappa_1 x_{F_i}}{\cos \theta_{e,i} \cos \psi_{e,i}}, \quad i = 1, \dots, n,$$

Time-Critical Coordinated Motion Control

Coordination Control Law

$$\begin{aligned} u_{\text{coord},1} &= -a \sum_{j \in J_1} (l'_1 - l'_j) + \frac{v_{d,1}}{l_{f1}} \\ u_{\text{coord},i} &= -a \sum_{j \in J_i} (l'_i - l'_j) + \chi_{I,i}, \quad i = 2, \dots, n \\ \dot{\chi}_{I,i} &= -b \sum_{j \in J_i} (l'_i - l'_j), \quad i = 2, \dots, n \end{aligned}$$

Speed Asssignment

Integral term

Communications Topology

$$\begin{aligned} u_{\text{coord}}(t) &= -aL(t)l'(t) + \begin{bmatrix} v_{d,1}(t)/l_{f1} \\ \chi_I(t) \end{bmatrix} \\ \dot{\chi}_I(t) &= -bCL(t)l'(t), \end{aligned}$$

Time-Critical Coordinated Motion Control

Key results (example)

Suppose the Graph satisfies

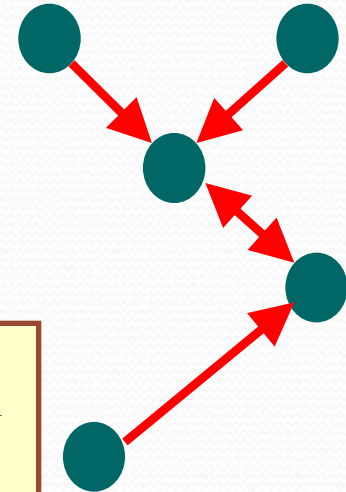
$$\frac{1}{T} \int_t^{t+T} x^T Q L(\tau) Q^T x \, d\tau \geq \mu, \quad \forall t \geq 0, \quad \forall x \in R^{n-1}$$

for some $T, \mu > 0$

(graph does not even have to be connected at any time!)



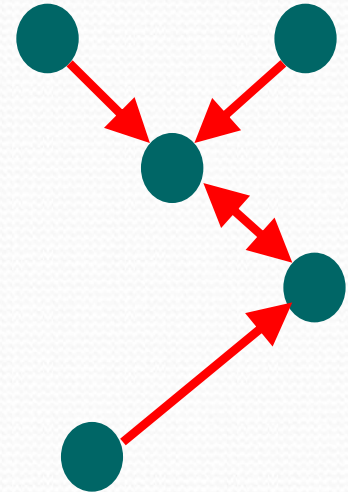
***“sensible” performance of the complete
Path Following + Coordination Controllers***



Time-Critical Coordinated Motion Control

$$\|\zeta(t)\| \leq k_1 \|\zeta(0)\| e^{-\lambda t} + k_2 \sup_{\tau \in [0, t)} |\dot{v}_{d,1}(\tau)|$$

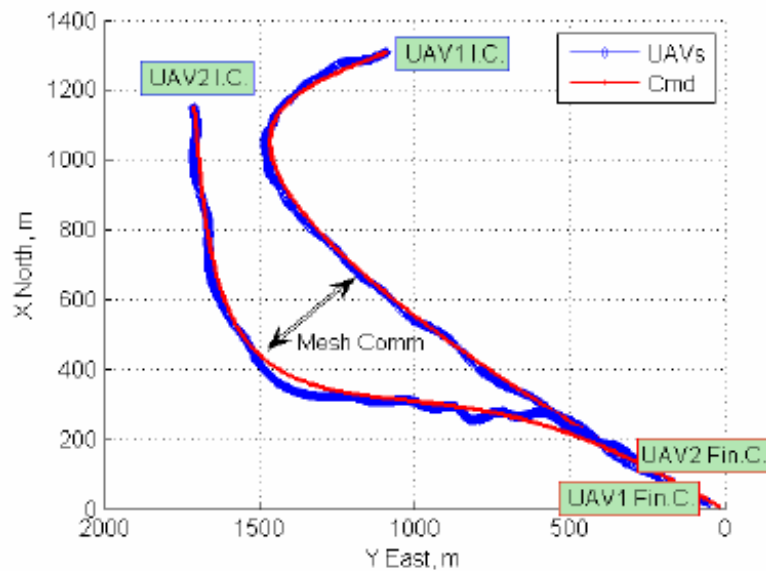
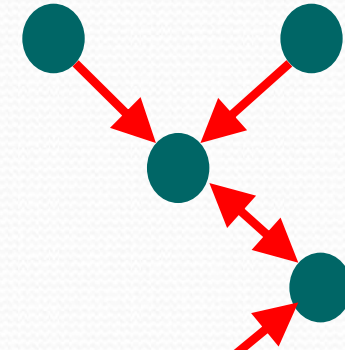
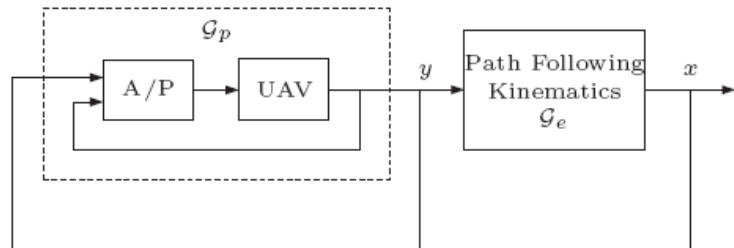
A function of normalized path lengths



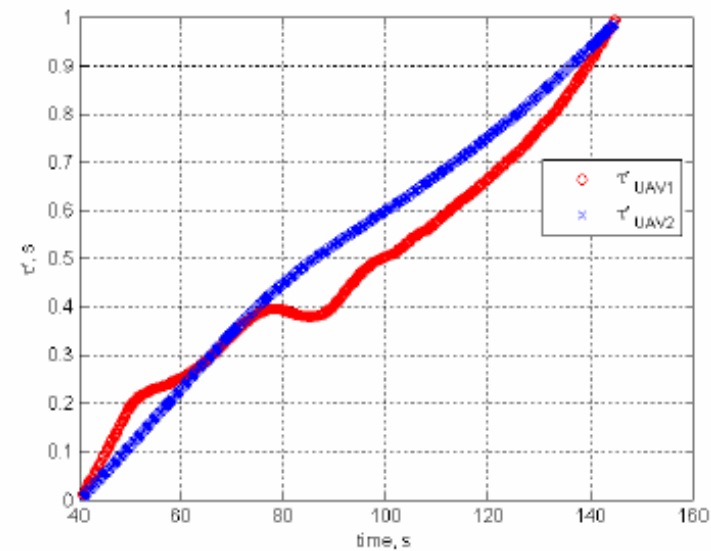
$$\limsup_{t \rightarrow \infty} |l'_i(t) - l'_j(t)| \leq k_4 \limsup_{t \rightarrow \infty} |\dot{v}_{d,1}(t)|$$

An ISS-like result

Time-Critical Coordinated Motion Control (HIL)

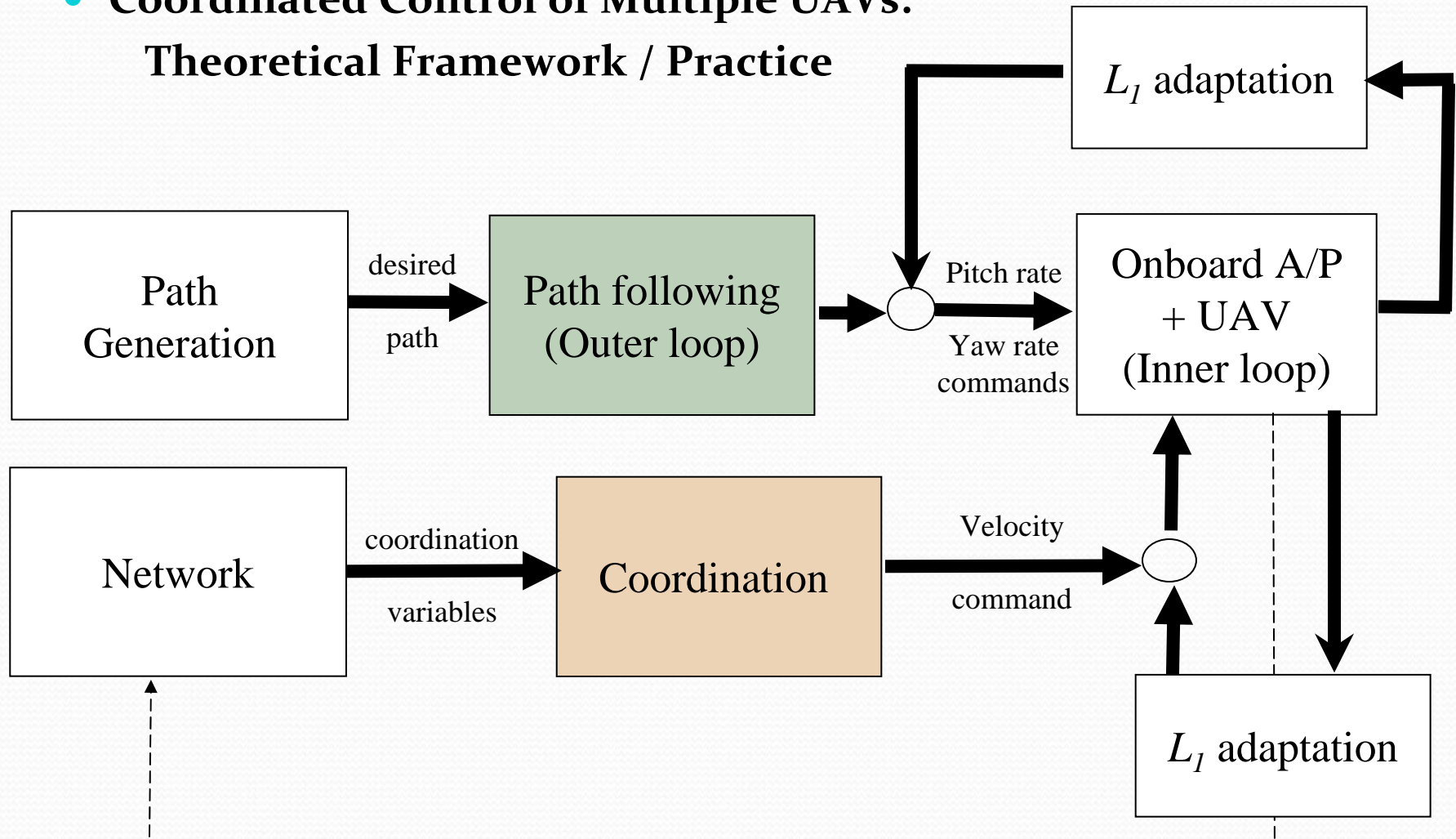


(a) UAV trajectories: 2D projection.

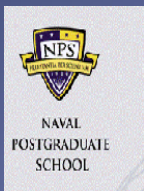


(b) Coordination states $l'_i(t)$.

- Coordinated Control of Multiple UAVs:
Theoretical Framework / Practice



Coordinated Path Following of Multiple UAVs for Time-Critical Missions in the Presence of Time-Varying Communication Topologies



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